

EXPONENTIAL ESTIMATES OF A CLASS OF TIME-DELAY NONLINEAR SYSTEMS WITH CONVEX REPRESENTATIONS

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This work introduces a novel approach to stability and stabilization of nonlinear systems with delayed multivariable inputs; it provides exponential estimates as well as a guaranteed cost of the system solutions. The result is based on an exact convex representation of the nonlinear system which allows a Lyapunov–Krasovskii functional to be applied in order to obtain sufficient conditions in the form of linear matrix inequalities. These are efficiently solved via convex optimization techniques. A real-time implementation of the developed approach on the twin rotor MIMO system is included.

Keywords: exponential estimates, time delay systems, TS model, guaranteed cost, convex representations.

1. Introduction

In the framework of control theory it is well known that the existence of a delay in the control signal can induce instability or poor performance. It is clear that most of real systems present some sort of time delay, whether perceptible or not, besides being inherently nonlinear. The presence of delays in the control system is a phenomenon that can be seen as the dead-time between transmission and execution of an action. In this context, the delay is due to the fact that forces affecting the dynamics are associated with past events.

Time delays can be found in networked and distributed systems (Murray, 2003), communication networks (Kelly, 2001), teleoperation (Anderson and Spong, 1989), telesurgery (Speich and Rose, 2004), unmanned aerial vehicles (Ramírez *et al.*, 2014), and decentralized control multiple collaborative agents (Beard *et al.*, 2006), synchronization and haptics (Cheong *et al.*, 2007), chemical processes (Marquez Rubio *et al.*, 2012), population dynamics (Gopalsamy, 1992), biological phenomena (Niculescu *et al.*, 2007), etc. Thus, the interest in understanding the effects of delays and in designing

stabilizing controllers that take those delays into account has been increasing. Correspondingly, controllers in the time-delay context have become more and more complex.

The stability analysis of time-delay systems has two main approaches: in the frequency domain and in the time domain. In the former, necessary and sufficient conditions of stability are given (see, e.g., Bellman and Cooke, 1963; El'sgol'ts, 1966). The first and main results on stability of time delay systems were given by Kabakov (1946), Tzypkin (1946) and Neimark (1973). The Nyquist and Michailov criteria are the most commonly used results (Hahn, 1967; La Salle and Lefschetz, 1961). As for the time-domain approach, we have found two variants: the Lyapunov-Razumikhin approach (Razumikhin, 1956), which is an adaptation of the classical Lyapunov theory, and the Lyapunov-Krasovskii one (Krasovskii, 1956), which is a natural extension of Lyapunov theory to enable the use of Lyapunov functionals (Duda, 2012). Further developments for observer design of time-delay systems can be also found (Thuan et al., 2012).

On the other hand, design of nonlinear control systems has benefited from convex structures since the seminal work of Taniguchi *et al.* (2001), which showed a methodology to obtain an exact convex representation

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of a nonlinear model in a compact set of the state space. It has been proved that this model shares the properties of the well-known Takagi–Sugeno (TS) model (Takagi and Sugeno, 1985) and can therefore be analyzed using the direct Lyapunov method (Tanaka and Sugeno, 1990); conditions thus obtained are usually expressed as linear matrix inequalities (LMIs) which can be efficiently solved via convex optimization techniques already implemented in commercially available software (Boyd *et al.*, 1994). A common structure for controller design under this approach has been the parallel distributed compensation (PDC), which employs the same convex functions of the model as to create a convex nonlinear controller that generalizes the ordinary state-feedback scheme (Wang *et al.*, 1996; Tanaka and Wang, 2001).

As expected, time-delay systems have been studied via convex structures, too; this has been done in order to take advantage of the systematic design procedures which guarantee computational tractability via LMIs (Lin et al., 1991). In the TS context, the last decade has witnessed an abundance of results on a variety of issues related to time-delay systems: stability using the Lyapunov-Razumikhin functional approach (Cao and Frank, 2001), stability criteria for a class of nonlinear stochastic systems with time delay (Wang et al., 2004; Li et al., 2011; Balasubramaniam et al., 2012), design of feedback controllers design for nonlinear interval time-delay systems via a T-S model (Chang et al., 2004), design of guaranteed cost control for T-S systems with delays (Chen and Liu, 2005; Chen et al., 2007b; 2007a; Kang and Wang, 2010) observer-based H-infinity control for time-delay T-S (Lin et al., 2007), α -dissipative control for T–S fuzzy descriptor systems with time delay (Gassaraa et al., 2014). Most of these results take advantage of the possibility of rewriting Lyapunov-Krasovskii functionals as convex expressions by inheritance of the model convex structure: this investigation follows that path. In contrast to ordinary "fuzzy" approaches like that of Liu et al. (2014), this work does not consider approximations but convex exact representations of nonlinear models.

Based on a novel form of the Lyapunov–Krasovskii functional, this paper provides conditions for exponential estimates (a decay rate) of a class of time-delay nonlinear systems as well as guaranteed control cost of the control input. This is a topic that has been addressed very recently in several works (Zhang *et al.*, 2009; Gassara *et al.*, 2010; Chiu and Chiang, 2011); in contrast to those, this report has the following features: (a) a matrix relaxation based on Finsler's lemma which allows a natural inclusion of slack variables; (b) an exact convex representation of the plant which makes the proposed results directly valid for the original nonlinear setup; (c) guaranteed control cost as well as exponential bounds in a single framework, specifically designed for delayed inputs. The results are organized as follows: Section 2 introduces the definitions and notation this work is based on; Section 3 presents the main contributions in two theorems: the first one considers stability under a given delayed PDC control law, while the second provides controller synthesis for stabilization with guaranteed control cost and exponential estimates; Section 4 illustrates the effectiveness of the proposed scheme via a simulation example as well as a real-time implementation on the well-known twin rotor MIMO system, whose fast dynamics are particularly sensitive to time delays on the control input; and Section 5 gathers some concluding remarks and suggestions for future work.

2. Preliminaries

Consider an affine-in-control nonlinear system whose input is delayed in time:

$$\dot{x}(t) = f(x(t))x(t) + g(x(t))u(t-\tau),$$

$$\phi(\theta) = x(\theta), \quad \theta \in [-\tau, 0],$$
(1)

where $f(\cdot) : \mathbb{R}^n \to \mathbb{R}^{n \times n}$ is a matrix function such that f(x(t))x(t) is a Lipschitz vector field, $g(\cdot) : \mathbb{R}^n \to \mathbb{R}^{n \times m}$ is a matrix function, $u(t) \in \mathbb{R}^m$ is the input vector, $\tau \in \mathbb{R}^+$ is a time delay, $\phi \in \mathfrak{C}([-\tau, 0], \mathbb{R}^n)$ is the initial function, and $\mathfrak{C}([-\tau, 0], \mathbb{R}^n)$ is the Banach space of real continuous functions on the interval $[-\tau, 0]$ with the following norm:

$$\|\phi\|_{\tau} := \max_{\theta \in [-\tau, 0]} \|\phi(\theta)\|,$$

with $\|\cdot\|$ being the Euclidean norm in \mathbb{R}^n . It is assumed that for each initial condition $\phi \in \mathfrak{C}([-\tau, 0], \mathbb{R}^n)$ and $t \ge 0$ there exists a unique solution $x(t;\phi)$ of the system. Here, $x_t(\phi) := \{x(t + \theta; \phi) : \theta \in [-\tau, 0]\} \in \mathbb{R}^n$ denote a segment of solution $x(t;\phi)$, and it is the state vector which is assumed to lie in a compact set \mathcal{C} . When it does not cause an ambiguity, we write x(t) and x_t instead of $x(t;\phi)$ and $x_t(\phi)$.

Results in this report are based on a convex rewriting of the nonlinear model (1). To this end, we will employ the sector nonlinearity methodology described by Taniguchi *et al.* (2001). If $f(\cdot)$ and $g(\cdot)$ have pnonlinearities, they can be grouped in a vector

$$z(\cdot) = \begin{bmatrix} z_1(\cdot) & z_2(\cdot) & \dots & z_p(\cdot) \end{bmatrix}^T$$

where each entry corresponds to a nonlinearity

$$z_j(\cdot) \in \left[\underline{z}_j, \overline{z}_j\right],$$
$$\underline{z}_j = \min_{x(t) \in \mathcal{C}} z_j(\cdot), \quad \overline{z}_j = \max_{x(t) \in \mathcal{C}} z_j(\cdot)$$

 $j \in \{1, 2, \dots, p\}$. The following weights are thus constructed:

$$w_0^j(\cdot) = \frac{\overline{z}_j - z_j(\cdot)}{\overline{z}_j - \underline{z}_j}, \quad w_1^j(\cdot) = 1 - w_0^j(\cdot), \qquad (2)$$

with $j \in \{1, 2, ..., p\}$. We can thus define the following functions:

$$h_{i} = h_{1+i_{1}+i_{2}\times 2+\ldots+i_{p}\times 2^{p-1}} = \prod_{j=1}^{p} w_{i_{j}}^{j}(z_{j}), \quad (3)$$

with $i \in \{1, 2, \ldots, r\}$, $r = 2^p$, $i_j \in \{0, 1\}$, which hold the convex-sum property $\sum_{i=1}^r h_i(\cdot) = 1$, $h_i(\cdot) \ge 0$, in \mathcal{C} .

Then, the nonlinear model (1) is rewritten in the following convex form:

$$\dot{x}(t) = \sum_{i=1}^{r} h_i \left(z(t) \right) \left(A_i x(t) + B_i u(t-\tau) \right), \quad (4)$$

$$\phi(\theta) = x(\theta), \quad \theta \in [-\tau, 0],$$

with $\phi(\theta)$ defined as before, $A_i = f(z(t)) |_{h_i=1}$, $B_i = g(z(t)) |_{h_i=1}$, $i \in \{1, 2, \ldots, r\}$. Sector nonlinearity guarantees that (4) is an exact representation of the nonlinear system described in (1) in C; it is not an approximation.

Some of the expressions in the sequel that involve convex sums will be written shortly as

$$\begin{split} \Upsilon_{z} &= \sum_{i=1}^{r} h_{i}\left(z(t)\right) \Upsilon_{i}, \\ \Upsilon_{zz} &= \sum_{i=1}^{r} \sum_{j=1}^{r} h_{i}\left(z(t)\right) h_{j}\left(z(t)\right) \Upsilon_{ij}, \\ \Upsilon_{z,\tau} &= \sum_{i=1}^{r} h_{i}\left(z(t-\tau)\right) \Upsilon_{i}, \\ \Upsilon_{zz}^{z,\tau} &= \sum_{i=1}^{r} \sum_{j=1}^{r} \sum_{k=1}^{r} h_{i}\left(z(t)\right) h_{j}\left(z(t)\right) h_{k}\left(z(t-\tau)\right) \Upsilon_{ij}^{k}. \end{split}$$

Following this notation, the convex model (4) can be written as $\dot{x}(t) = A_z x(t) + B_z u(t - \tau)$.

In order to obtain LMI conditions, MFs should be removed from nested convex sums. The following result will be employed to perform this task in triple convex sums, one of which will be delayed: it is an immediate extension of the relaxation lemma of Tuan *et al.* (2001):

Lemma 1. (Relaxation lemma) (Tuan *et al.*, 2001) Let Υ_{ij}^k be matrices of proper dimensions. Then $\Upsilon_{zz}^{z,\tau} < 0$ is implied by

$$\begin{aligned}
\Upsilon_{ii}^{k} &< 0, \quad \forall (i,k) \in \{1,2,\dots,r\}^{2}, \\
\frac{2}{r-1}\Upsilon_{ii}^{k} + \Upsilon_{ij}^{k} + \Upsilon_{ji}^{k} < 0, \\
\forall (i,j,k) \in \{1,2,\dots,r\}^{3}, i \neq j.
\end{aligned}$$
(5)

The following control law corresponds to the well-known parallel distributed compensation (PDC) (Wang *et al.*, 1996) and will be employed in the sequel:

$$u(t) = \sum_{j=1}^{r} h_i(z(t)) K_j x(t) = K_z x(t), \qquad (6)$$

with $K_i \in \mathbb{R}^{m \times n}$, $i \in \{1, 2, ..., r\}$, being controller gains to be determined later. It is important to stress the fact that this control law is nonlinear because functions $h_i(\cdot)$ may depend nonlinearly on the states.

Substituting (6) in (4), the following closed-loop system equation is obtained:

$$\dot{x}(t) = A_z x(t) + B_z K_{z,\tau} x(t-\tau),$$

$$\phi(\theta) = x(\theta), \quad \theta \in [-\tau, 0],$$
(7)

where $K_{z,\tau} = \sum_{j=1}^{r} h_j (z(t-\tau)) K_j$.

For brevity, symmetric terms in matrix expressions as well as in-line expressions will be denoted with a star (*). Should a matrix expression be involved with symbols ">" and "<", they will stand for positive and negative-definiteness, respectively. Arguments will be omitted when convenient.

The following matrix property will play a central role in obtaining the LMI conditions in this work.

Lemma 2. (Finsler's lemma) (Oliveira and Skelton, 2001) Let $x \in \mathbb{R}^n$, $Q = Q^T \in \mathbb{R}^{n \times n}$, and $R \in \mathbb{R}^{m \times n}$ such that rank(R) < n. The following expressions are equivalent:

- 1. $x^T Q x < 0, \forall x \in \{x \in \mathbb{R}^n : x \neq 0, \Gamma x = 0\},\$
- 2. $\exists \Omega \in \mathbb{R}^{n \times m} : Q + \Omega \Gamma + \Gamma^T \Omega^T < 0.$

We now turn our attention to the definition of guaranteed control cost and exponential estimates. For the first one, let $W \in \mathbb{R}^{n \times n}$, $W = W^T > 0$ and $S \in \mathbb{R}^{m \times m}$, $S = S^T > 0$; then, the following cost function will be used in the sequel (Chen *et al.*, 2007a):

$$J = \int_0^\infty (x^T(t)Wx(t) + u^T(t-\tau)Su(t-\tau)) \,\mathrm{d}t.$$
 (8)

Guaranteed control cost control law. (Yu and Chu, 1999) For a nonlinear system of the form (1) (or, equivalently, (4)), if there exists a control input u(t), a constant J_0 such that the closed-loop system is asymptotically stable, and $J \leq J_0$, where J is given by (8), then J_0 is said to be a guaranteed cost and the control input u(t) is called a guaranteed control cost control law for the system (1) (or, equivalently, (4)).

As for exponential estimates, the following result relating them with a Lyapunov–Krasovskii functional will be used.

Theorem 1. (Kharitonov and Hinrichsen, 2004) *Consider* the nonlinear system (1) or, equivalently, its convex TS representation (4). If there exist a functional $V(\cdot)$ and positive constants α_1 , α_2 , and σ such that

1.
$$\alpha_1 ||x(t)||^2 \le V(x_t) \le \alpha_2 ||x_t||_{\tau}^2$$
,
2. $\dot{V}(x_t) + 2\sigma V(x_t) < 0$,

then the solutions $x(t; \phi)$ of the system (1) (or, equivalently, (4)) satisfy the exponential estimates

$$||x(t;\phi)|| \le \sqrt{\frac{\alpha_2}{\alpha_1}} e^{-\sigma t} ||\phi||_{\tau}.$$

3. Main results

3.1. Stability. We begin by considering the stability analysis of the closed-loop time-delay system (7), which means that gains K_j , $j \in \{1, 2, ..., r\}$ are already known. When stability analysis is performed, it is customary to provide these gains such that terms $A_i + B_i K_i$, $j \in \{1, 2, ..., r\}$ are Hurwitz; of course, this does not guarantee the stability of the whole scheme, which is why the stability analysis comes at hand. The next theorem should be therefore considered a first step towards the controller synthesis methodology shown in the next subsection.

Theorem 2. The closed-loop nonlinear system (7) with a time-delay $\mathbb{R} \ni \tau > 0$ is exponentially stable with guaranteed cost

$$J_0 = x^T(0)Px(0) + \int_{-\tau}^0 x^T(s)Qe^{2\sigma s}x(s) \,\mathrm{d}s + \tau \int_{-\tau}^0 \int_{\theta}^0 \dot{x}^T(s)Re^{2\sigma s}\dot{x}(s) \,\mathrm{d}s \,\mathrm{d}\theta$$
(9)

for the cost function (8) with Q, P, $R \in \mathbb{R}^{n \times n}$ such that $Q = Q^T > 0$, $P = P^T > 0$, $R = R^T > 0$, and holds exponential estimates

$$||x(t;\phi)|| \le \sqrt{\frac{\alpha_2}{\alpha_1}} e^{-\sigma t} ||\phi||_{\tau}, \tag{10}$$

for a decay rate $\mathbb{R} \ni \sigma > 0$ with $\alpha_1 = \lambda_{\min}(P)$, $\alpha_2 = \lambda_{\max}(P) + \lambda_{\max}(Q)\tau + \lambda_{\max}(R)\tau$, if there exist matrices $W \in \mathbb{R}^{n \times n} : W = W^T > 0$, $S \in \mathbb{R}^{m \times m} : S = S^T > 0$, $K_j \in \mathbb{R}^{m \times n}$, H_i^p , $N_{ij}^p \in \mathbb{R}^{n \times n}$, $i, j \in \{1, 2, ..., r\}$, $p \in \{1, 2, 3\}$ satisfying LMIs (5) for

$$\Upsilon_{ij}^{k} = \begin{bmatrix} \psi_{11} & \psi_{12} & \psi_{13} & \psi_{14} & 0\\ (*) & \psi_{22} & \psi_{23} & \psi_{24} & K_{k}^{T}\\ (*) & (*) & \psi_{33} & \psi_{34} & 0\\ (*) & (*) & (*) & \psi_{44} & 0\\ 0 & (*) & 0 & 0 & -S^{-1} \end{bmatrix}, \quad (11)$$

where $i, j, k \in \{1, 2, ..., r\}$, and $\psi_{11} = H^{\frac{1}{2}}A_i + N^{\frac{1}{2}} + (*) + 2P\sigma + Q + W_i$

$$\begin{split} \psi_{11} &= H_j \, A_i + N_{ij} + (*) + 2I \, 0 + Q + W, \\ \psi_{12} &= H_j^1 B_i K_k + A_i^T \left(H_j^2\right)^T - N_{ij}^1 + \left(N_{ij}^2\right)^T, \\ \psi_{13} &= -H_j^1 + A_i^T \left(H_j^3\right)^T + \left(N_{ij}^3\right)^T + P, \\ \psi_{14} &= N_{ij}^1, \\ \psi_{22} &= H_j^2 B_i K_k - N_{ij}^2 + (*) - Q e^{2\sigma\tau}, \\ \psi_{23} &= -H_j^2 + K_k^T B_i^T \left(H_j^3\right)^T - \left(N_{ij}^3\right)^T, \\ \psi_{24} &= N_{ij}^2, \\ \psi_{33} &= \tau^2 R - H_j^3 - \left(H_j^3\right)^T, \\ \psi_{34} &= N_{ij}^3, \\ \psi_{44} &= -R e^{-2\sigma\tau}. \end{split}$$

Proof. Consider the Lyapunov–Krasovskii functional of the form (Mondie and Kharitonov, 2005)

$$V(x_t) = x^T(t)Px(t) + \int_{t-\tau}^t x^T(s)Qe^{2\sigma(s-t)}x(s) ds + \tau \int_{-\tau}^0 \int_{t+\theta}^t \dot{x}^T(s)Re^{2\sigma(s-t)}\dot{x}(s) ds d\theta.$$
(12)

Clearly, the above functional satisfies the following quadratics bounds:

$$\alpha_1 ||x(t)||^2 \le V(x_t) \le \alpha_2 ||x_t||_{\tau}^2, \tag{13}$$

where $\alpha_1 = \lambda_{\min}(P)$ and $\alpha_2 = \lambda_{\max}(P) + \lambda_{\max}(Q)\tau + \lambda_{\max}(R)\tau$. We now turn our attention to the time derivative of (12):

$$\begin{split} \dot{V}(x_t) &= 2x^T(t)P\dot{x}(t) + x^T(t)Qx(t) \\ &- x^T(t-\tau)Qe^{-2\sigma\tau}x(t-\tau) \\ &- 2\sigma\int_{t-\tau}^t x^T(s)Qe^{2\sigma(s-t)}x(s)\,\mathrm{d}s \\ &+ \tau^2\dot{x}^T(t)R\dot{x}(t) \\ &- \tau\int_{t-\tau}^t \dot{x}^T(s)Re^{2\sigma(s-t)}\dot{x}(s)\,\mathrm{d}s \\ &- 2\sigma\tau\int_{-\tau}^0\int_{t+\theta}^t \dot{x}^T(s)Re^{2\sigma(s-t)}\dot{x}(s)\,\mathrm{d}s\,\mathrm{d}\theta. \end{split}$$

Condition 2 in Theorem 1 translates into

$$\dot{V} + 2\sigma V$$

$$= 2x^{T}(t)P\dot{x}(t) + 2\sigma x^{T}(t)Px(t)$$

$$+ x^{T}(t)Qx(t) - x^{T}(t-\tau)Qe^{-2\sigma\tau}x(t-\tau)$$

$$+ \tau^{2}\dot{x}^{T}(t)R\dot{x}(t)$$

$$-\tau \int_{t-\tau}^{t} \dot{x}^{T}(s) Re^{2\sigma(s-t)} \dot{x}(s) ds$$

= $\bar{x}^{T} \begin{bmatrix} 2\sigma P + Q & 0 & P \\ 0 & -Qe^{-2\sigma\tau} & 0 \\ P & 0 & \tau^{2}R \end{bmatrix} \bar{x}$
 $-\tau \int_{t-\tau}^{t} \dot{x}^{T}(s) Re^{2\sigma(s-t)} \dot{x}(s) ds < 0, \qquad (14)$

where $\bar{x} = \begin{bmatrix} x^T(t) & x^T(t-\tau) & \dot{x}^T(t) \end{bmatrix}^T$. In this context, the convex model (7) can be rewritten as

$$\begin{bmatrix} A_z & B_z K_{z,\tau} & -I \end{bmatrix} \begin{bmatrix} x(t) \\ x(t-\tau) \\ \dot{x}(t) \end{bmatrix} = 0, \quad (15)$$

whereas the fundamental theorem of calculus can be put in a similar fashion as follows:

$$\begin{bmatrix} I & -I & 0 \end{bmatrix} \begin{bmatrix} x(t) \\ x(t-\tau) \\ \dot{x}(t) \end{bmatrix} - \int_{t-\tau}^{t} \dot{x}(s) \, \mathrm{d}s = 0. \quad (16)$$

Finsler's lemma will be applied twice to combine the inequality (14) and the restrictions (15) and (16); it is important to notice that the integral terms in (14) and (16) will be included in Finsler's equivalence without loss of generality. Thus, after applying Finsler's lemma with the inequality (14) and the restriction (15), we have

$$\bar{x}^{T} \left(\begin{bmatrix} H_{z}^{1} \\ H_{z}^{2} \\ H_{z}^{3} \end{bmatrix} \begin{bmatrix} A_{z} & B_{z}K_{z,\tau} & -I \end{bmatrix} + (*) \\ + \begin{bmatrix} 2\sigma P + Q & 0 & P \\ 0 & -Qe^{-2\sigma\tau} & 0 \\ P & 0 & \tau^{2}R \end{bmatrix} \right) \bar{x} \\ -\tau \int_{t-\tau}^{t} \dot{x}^{T}(s)Re^{2\sigma(s-t)}\dot{x}(s) \, \mathrm{d}s \\ = \bar{x}^{T}\Phi_{0}\bar{x} \\ -\tau \int_{t-\tau}^{t} \dot{x}^{T}(s)Re^{2\sigma(s-t)}\dot{x}(s) \, \mathrm{d}s < 0,$$
(17)

with Φ_0 given in (18), H_z^p , $p \in \{1, 2, 3\}$ being single convex sums of matrices $H_j^p \in \mathbb{R}^{n \times n}$, $p \in \{1, 2, 3\}$, $j \in \{1, \ldots, r\}$. Notice that

$$\begin{bmatrix} \left(H_z^1\right)^T & \left(H_z^2\right)^T & \left(H_z^3\right)^T \end{bmatrix}^T$$

operates as Ω in Finsler's lemma (statement 1).

We now reapply Finsler's lemma with (17) as the new

inequality and (16) as the new restriction. This yields

$$\begin{split} \bar{x}^{T} \left(\begin{bmatrix} N_{zz}^{1} \\ N_{zz}^{2} \\ N_{zz}^{3} \end{bmatrix} \begin{bmatrix} I & -I & 0 \end{bmatrix} + (*) + \Phi_{0} \right) \bar{x} \\ & - \bar{x}^{T} \begin{bmatrix} N_{zz}^{1} \\ N_{zz}^{2} \\ N_{zz}^{3} \end{bmatrix} \int_{t-\tau}^{t} \dot{x}(s) \, \mathrm{d}s - \int_{t-\tau}^{t} \dot{x}(s) \, \mathrm{d}s \begin{bmatrix} N_{zz}^{1} \\ N_{zz}^{2} \\ N_{zz}^{3} \end{bmatrix}^{T} \bar{x} \\ & - \tau \int_{t-\tau}^{t} \dot{x}^{T}(s) Re^{2\sigma(s-t)} \dot{x}(s) \, \mathrm{d}s \\ & = \bar{x}^{T} \left(\begin{bmatrix} N_{zz}^{1} + (N_{zz}^{1})^{T} & (N_{zz}^{2})^{T} - N_{zz}^{1} & (N_{zz}^{3})^{T} \\ N_{zz}^{2} - (N_{zz}^{1})^{T} & -N_{zz}^{2} - (N_{zz}^{2})^{T} - (N_{zz}^{3})^{T} \end{bmatrix} \\ & + \Phi_{0} \right) \bar{x} - 2\bar{x}^{T} \begin{bmatrix} N_{zz}^{1} \\ N_{zz}^{2} \\ N_{zz}^{3} \end{bmatrix} \int_{t-\tau}^{t} \dot{x}(s) \, \mathrm{d}s \\ & - \tau \int_{t-\tau}^{t} \dot{x}^{T}(s) Re^{2\sigma(s-t)} \dot{x}(s) \, \mathrm{d}s < 0, \end{split}$$
(19)

with N_{zz}^p , $p \in \{1, 2, 3\}$ being double convex sums of matrices $N_{ij}^p \in \mathbb{R}^{n \times n}$, $p \in \{1, 2, 3\}$, $i, j \in \{1, \ldots, r\}$. Once again, notice that

$$N = \begin{bmatrix} \left(N_{zz}^1 \right)^T & \left(N_{zz}^2 \right)^T & \left(N_{zz}^3 \right)^T \end{bmatrix}^T$$

takes the place of Ω in Finsler's lemma (statement 1); notice also that the restriction in this case is extended from $\Gamma \bar{x} = 0$ to the form $\Gamma_1 \bar{x} + \Gamma_2 = 0$, where Γ_1 is the matrix term multiplied by \bar{x} in (16) and Γ_2 is the integral term in the same expression. By the Park and Jensen inequalities (Gu *et al.*, 2003), we have

$$-2\bar{x}^{T}(t)N\int_{t-\tau}^{t}\dot{x}(s)\,\mathrm{d}s$$

$$\leq \bar{x}^{T}(t)NR^{-1}e^{2\sigma\tau}N^{T}\bar{x}(t)$$

$$+\int_{t-\tau}^{t}\dot{x}^{T}(s)\,\mathrm{d}sRe^{-2\sigma\tau}\int_{t-\tau}^{t}\dot{x}(s)\,\mathrm{d}s$$

$$\leq \bar{x}^{T}(t)NR^{-1}e^{2\sigma\tau}N^{T}\bar{x}(t)$$

$$+\tau\int_{t-\tau}^{t}\dot{x}^{T}(s)Re^{-2\sigma\tau}\dot{x}(s)\,\mathrm{d}s, \qquad (20)$$

which can be taken into account to cancel out the last integral term in (19) yielding

$$\bar{x}^{T} \left(\Phi_{0} + \Phi_{1} + NR^{-1}e^{2\sigma\tau}N^{T} \right) \bar{x} < 0, \quad (21)$$

with

$$\Phi_{1} = \begin{bmatrix} N_{zz}^{1} + (N_{zz}^{1})^{T} & (N_{zz}^{2})^{T} - N_{zz}^{1} & (N_{zz}^{3})^{T} \\ N_{zz}^{2} - (N_{zz}^{1})^{T} & -N_{zz}^{2} - (N_{zz}^{2})^{T} - (N_{zz}^{3})^{T} \\ N_{zz}^{3} & -N_{zz}^{3} & 0 \end{bmatrix}.$$

The following development intends to include the guaranteed control cost in the previous analysis. To this

end, consider matrices $\mathbb{R}^{n \times n} \ni W > 0$ and $S \in \mathbb{R}^{m \times m}$: S > 0 from the integral argument in the cost function (8) by substituting (6):

$$x^{T}(t)Wx(t) + u^{T}(t-\tau)Su(t-\tau) = x^{T}(t)Wx(t) + x^{T}(t-\tau)K_{z,\tau}^{T}SK_{z,\tau}x(t-\tau) = \bar{x}^{T}(t)\Phi_{2}\bar{x}(t),$$
(22)

with

$$\Phi_2 = \begin{bmatrix} W & 0 & 0 \\ 0 & K_{z,\tau}^T S K_{z,\tau} & 0 \\ 0 & 0 & 0 \end{bmatrix}.$$

The inequality (21) guarantees that $\dot{V}+2\sigma V < 0$; keeping this in mind, as well as the equivalence in (22), it follows that

$$x^{T}(t)Wx(t) + u^{T}(t-\tau)Su(t-\tau)$$

= $x^{T}(t)Wx(t) + u^{T}(t-\tau)Su(t-\tau) + \dot{V} - \dot{V}$
< $x^{T}(t)Wx(t) + u^{T}(t-\tau)Su(t-\tau)$
+ $2\sigma V + \dot{V} - \dot{V}$
< $\bar{x}^{T}(t)(\Phi_{0} + \Phi_{1} + \Phi_{2} + NR^{-1}e^{2\sigma\tau}N^{T})\bar{x}(t)$
- $\dot{V}.$ (23)

By the Schur complement we have that $\Phi_0 + \Phi_1 + \Phi_2 + NR^{-1}e^{2\sigma\tau}N^T < 0$ is equivalent to

$$\begin{bmatrix} \Phi_0 + \Phi_1 + \Phi_2 & N \\ N^T & -Re^{-2\sigma\tau} \end{bmatrix} < 0.$$

If $[\Phi_0]_{2,2} + [\Phi_1]_{2,2} + [\Phi_2]_{2,2} = [\Phi_0]_{2,2} + [\Phi_1]_{2,2} + K_{z,\tau}^T S K_{z,\tau}$ denotes the block entry (2, 2) of the previous matrix, the Schur complement can be applied again yielding Eqn. (24). By the relaxation lemma, it is now clear that (24) holds if the LMIs (5) are satisfied for Υ_{ij}^k , $i, j, k \in \{1, 2, ..., r\}$ as defined in (11).

We can now return to the guaranteed cost function. Since $\dot{V} + 2\sigma V < 0$ and bounds given on (13) have been established, Theorem 1 guarantees that solutions of the closed-loop model (7) satisfy (10). On the other hand, note that (24) guarantees $\Phi_0 + \Phi_1 + \Phi_2 + NR^{-1}e^{2\sigma\tau}N^T < 0$; therefore, (23) is guaranteed if

$$x^{T}(t)Wx(t) + u^{T}(t-\tau)Su(t-\tau) \le -\dot{V}.$$
 (25)

Integrating (25) on the interval [0, T], we have

$$\begin{split} &\int_0^T (x^T(t)Wx(t) + u^T(t-\tau)Su(t-\tau))\,\mathrm{d}t\\ &\leq -V(T) + V(0)\\ &= -V(T) + x^T(0)Px(0) + \int_{-\tau}^0 x^T(s)Qe^{2\sigma s}x(s)\,\mathrm{d}s\\ &+ \tau \int_{-\tau}^0 \int_{\theta}^0 \dot{x}^T(s)Re^{2\sigma s}\dot{x}(s)\,\mathrm{d}s\,\mathrm{d}\theta. \end{split}$$

Since $\dot{V} < 0, V(t) > 0$ and $\exists V(T) > 0$ as $T \to \infty$, we get

$$\begin{split} &\int_0^\infty (x^T(t)Wx(t) + u^T(t-\tau)Su(t-\tau))\,\mathrm{d}t\\ &\leq x^T(0)Px(0) + \int_{-\tau}^0 x^T(s)Qe^{2\sigma s}x(s)\,\mathrm{d}s\\ &+ \tau \int_{-\tau}^0 \int_{\theta}^0 \dot{x}^T(s)Re^{2\sigma s}\dot{x}(s)\,\mathrm{d}s\,\mathrm{d}\theta, \end{split}$$

which means that the guaranteed cost (9) is satisfied, thus completing the proof.

Remark 1. Note that, traditionally, the constraints (15) and (16) are incorporated in the Lyapunov time-derivative (14) via zero additions instead of Finsler's lemma (Chen *et al.*, 2007a). Nevertheless, both the approaches lead to the same results.

3.2. Stabilization. Theorem 1 assumes the gains K_i , $i \in \{1, 2, ..., r\}$, are already given: it therefore performs a stability analysis. The next result provides sufficient conditions for stabilization (i.e., controller synthesis) of a nonlinear model of the form (1) under a delayed control law. As before, the result is obtained through a convex rewriting (4) of the original model (1), provided the control law (6) also shares the convex structure of this representation.

Theorem 3. The closed-loop nonlinear system (7) with time delay $\mathbb{R} \ni \tau > 0$ is exponentially stable with guaranteed cost J_0 in (9) for the cost function (8) and holds the exponential estimates (10) for a decay rate $\mathbb{R} \ni \sigma > 0$ with $\alpha_1 = \lambda_{\min}(P)$, $\alpha_2 = \lambda_{\max}(P) + \lambda_{\max}(Q)\tau + \lambda_{\max}(R)\tau$, if there exist matrices $\bar{Q}, \bar{P}, \bar{R}, W \in \mathbb{R}^{n \times n}$ such that $\bar{Q} = \bar{Q}^T > 0$, $\bar{P} = \bar{P}^T > 0$, $W = W^T > 0$, $\mathbb{R}^{m \times m} \ni S = S^T > 0$, $Y \in \mathbb{R}^{n \times n}$, $F_k \in \mathbb{R}^{m \times n}$,

$$\Phi_{0} = \begin{bmatrix} H_{z}^{1}A_{z} + (*) + 2\sigma P + Q & H_{z}^{1}B_{z}K_{z,\tau} + A_{z}^{T} \left(H_{z}^{2}\right)^{T} & P - H_{z}^{1} + A_{z}^{T} \left(H_{z}^{3}\right)^{T} \\ (*) & H_{z}^{2}B_{z}K_{z,\tau} + (*) - Qe^{-2\sigma\tau} & -H_{z}^{2} + K_{z,\tau}^{T}B_{z}^{T} \left(H_{z}^{3}\right)^{T} \\ (*) & (*) & \tau^{2}R - H_{z}^{3} - \left(H_{z}^{3}\right)^{T} \end{bmatrix}.$$
(18)

$$\Upsilon_{zz}^{z,\tau} = \begin{bmatrix} \Phi_0 + \Phi_1 + \begin{bmatrix} W & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} & \begin{bmatrix} N_{zz}^1 \\ N_{zz}^2 \\ N_{zz}^3 \\ N_{zz}^3 \end{bmatrix} & \begin{bmatrix} 0 \\ K_{z,\tau}^T \\ 0 \\ 0 \end{bmatrix} \\ (*) & -Re^{-2\sigma\tau} \end{bmatrix} & \begin{bmatrix} 0 \\ K_{z,\tau}^T \\ 0 \\ 0 \end{bmatrix} \\ < 0.$$
(24)

 $k \in \{1, 2, \dots, r\}, \bar{N}_p \in \mathbb{R}^{n \times n}, p \in \{1, 2, 3\}, and constants <math>a_2, a_3 \in \mathbb{R}$, satisfying

$$\begin{bmatrix} \psi_{11} & \psi_{12} & \psi_{13} & \psi_{14} & 0 & \psi_{16} \\ (*) & \psi_{22} & \psi_{23} & \psi_{24} & \psi_{25} & 0 \\ (*) & (*) & \psi_{33} & \psi_{34} & 0 & 0 \\ (*) & (*) & (*) & \psi_{44} & 0 & 0 \\ (*) & (*) & (*) & (*) & \psi_{55} & 0 \\ (*) & (*) & (*) & (*) & (*) & \psi_{66} \end{bmatrix} < 0, \quad (26)$$

where $i, k \in \{1, 2, ..., r\}$ *, and*

$$\begin{split} \bar{\psi_{11}} &= A_i Y^T + Y A_i^T + \bar{N_1} + \bar{N_1}^T \\ &\quad + 2\sigma \bar{P} + \bar{Q}, \\ \bar{\psi_{12}} &= B_i F_k + a_2 Y A_i^T - \bar{N_1} + \bar{N_2}^T, \\ \bar{\psi_{13}} &= -Y^T + a_3 Y A_i^T + \bar{N_3}^T + \bar{P}, \\ \bar{\psi_{14}} &= \bar{N_1}, \\ \bar{\psi_{16}} &= Y, \\ \bar{\psi_{16}} &= Y, \\ \bar{\psi_{16}} &= Y, \\ \bar{\psi_{16}} &= Z \\ &\quad - \bar{N_2}^T - \bar{Q} e^{2\sigma\tau}, \\ \bar{\psi_{23}} &= -a_2 Y^T + a_3 F_k^T B_i^T - \bar{N_3}^T, \\ \bar{\psi_{24}} &= \bar{N_2}, \\ \bar{\psi_{25}} &= F_k^T, \\ \bar{\psi_{33}} &= -a_3 Y^T - a_3 Y + \tau^2 \bar{R}, \\ \bar{\psi_{34}} &= \bar{N_3}, \\ \bar{\psi_{44}} &= -\bar{R} e^{-2\sigma\tau}, \\ \bar{\psi_{55}} &= -S^{-1}, \\ \bar{\psi_{66}} &= -W^{-1}. \end{split}$$

The controller gains in (6) are thus calculated as $K_k = F_k Y^{-T}$, $k \in \{1, 2, ..., r\}$. The matrices corresponding to the Lyapunov–Krasovskii functional (12) are calculated as $P = Y^{-1}\bar{P}Y^{-T}$, $Q = Y^{-1}\bar{Q}Y^{-T}$ and $R = Y^{-1}\bar{R}Y^{-T}$.

Proof. Gains in (11) are multiplied by different sets of matrices H_j^p . In order to accomplish controller synthesis, these matrices are uniformized by choosing them as $H_j^1 = H_1$, $H_j^2 = a_2H_1$, and $H_j^3 = a_3H_1$, with $H_1 \in \mathbb{R}^{n \times n}$ invertible and real constants a_2 , a_3 . This makes the same-instant crossed terms in (11) disappear; therefore, matrices N_{ij}^p are also reduced as $N_{ij}^1 = N_1$, $N_{ij}^2 = N_2$, and $N_{ij}^3 = N_3$, for $N_1, N_2, N_3 \in \mathbb{R}^{n \times n}$.

Let $Y = H_1^{-1}$. The desired result easily arises after three steps:

- 1. Rewrite the expression (11) with the aforementioned reductions.
- 2. Pre- and post-multiply (11) by

block-diag
$$\begin{bmatrix} Y & Y & Y & I \end{bmatrix}$$

and its transpose, respectively.

3. For the resulting expression, take the Schur complement of the block-entry (1, 1) over the term YWY^T .

Hence, the expression (26) arises, thus concluding the proof.

Remark 2. Notice that only indexes i and k remain in the expression, and that index k corresponds to gains K_k which occur at a different instant than indexes i from the system, due to the time delay; therefore, no relaxation lemma can be applied here and *all* the combinations (i, k)should be tested.

Remark 3. Theorem 3 is applicable to time-delay nonlinear systems *exactly* represented in the convex TS form via the sector nonlinearity approach (Taniguchi *et al.*, 2001). This representation is *not* an approximation of the original model as happens with many other "fuzzy" methodologies such as that by Liu *et al.* (2014), which rely on fuzzy structures that are not fired simultaneously.

Remark 4. Convex structures in matrices Q and R of the Lyapunov–Krasovskii functional (12) can be easily exploited, since their time derivative will not include the time derivatives of the MFs $h_i(\cdot)$, i.e.,

$$V(x_t)$$

$$= x^T(t)Px(t) + \int_{t-\tau}^t x^T(s)Q_z e^{2\sigma(s-t)}x(s) ds$$

$$+ \tau \int_{-\tau}^0 \int_{t+\theta}^t \dot{x}^T(s)R_z e^{2\sigma(s-t)}\dot{x}(s) ds d\theta,$$
(28)

with $Q_z = \sum_{i=1}^r h_i(z)Q_i$ and $R_z = \sum_{i=1}^r h_i(z)R_i$. Clearly, this may provide additional degrees of freedom to relax the aforementioned results (Liu *et al.*, 2014).

4. Implementation on the twin rotor MIMO system

In order to illustrate the applicability of the proposed approach in a real-time application whose behavior is highly sensitive to time delays, this section considers the twin rotor MIMO system (TRMS) (Fee, 1998). Most of the state-space representations of the TRMS have 6 states (Nejjari et al., 2011; Pratap and Purwar, 2010; Tao et al., 2010): the elevation and azimuth angles, their corresponding angular speeds, and the motor speeds. Some other models add a coupling internal state; this is the case of the TRMS model employed in this investigation (Fee, 1998; Ahmed et al., 2009; Gonzalez et al., 2012). Thus, considering x_1 to be the main motor speed, x_2 the elevation angle, x_3 the elevation angular speed, x_4 the tail motor speed, x_5 the azimuth angle, x_6 the azimuth angular speed, and x_7 a coupling internal state, the TRMS model is given by (Fee, 1998; Gonzalez et al., 2012)

$$\dot{x}(t) = f(x)x(t) + g(x)u(t),$$
 (29)

with $x(t) = \begin{bmatrix} x_1 & x_2 & x_3 & x_4 & x_5 & x_6 & x_7 \end{bmatrix}^T$ being the state vector, $u(t) \in \mathbb{R}^{2 \times 1}$ being the input vector (recall the system has two actuators corresponding to the motors torque), and

$$\begin{split} f(x) &= \begin{bmatrix} -0.83 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ E_1(x) & E_2(x) & -\frac{0.006}{I_1} & 0 & 0 & E_3(x) & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & E_4(x) & 0 & -\frac{0.1}{I_2} & -\frac{1}{I_2} \\ E_5(x) & 0 & 0 & 0 & 0 & 0 & 0 & -0.5 \end{bmatrix}, \\ g(x) &= \begin{bmatrix} 0.917 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ E_6(x) & 0 \end{bmatrix}, \\ E_1(x) &= (b_1 + a_1x_1) \left(\frac{1 - 0.05x_6 \cos x_2}{I_1} \right), \\ E_2(x) &= -\frac{0.32 \sin x_2}{I_1x_2}, \\ E_3(x) &= \frac{0.0163x_6 \sin (2x_2)}{I_1}, \\ E_4(x) &= \frac{b_2 + a_2x_4}{I_2}, \\ E_5(x) &= -0.1 (b_1 + a_1x_1) + 0.583 \left(\frac{b_1}{2} + a_1x_1 \right), \\ E_6(x) &= \frac{1.1A_{cte}}{I_2} \left(\frac{b_1}{2} + a_1x_1 \right), \end{split}$$

 $A_{cte} = -0.7, a_1 = 0.0135, a_2 = 0.02, b_1 = 0.0924, b_2 = 0.09, I_1 = 0.068, \text{ and } I_2 = 0.02.$

An exact convex representation of the nonlinear model (29) can be found through the sector nonlinearity approach described in Section 2 by taking $z_i \in [\underline{z}_i, \overline{z}_i]$ as

$$z_1 = x_1 \in [-0.8, 0.8],$$

$$z_2 = x_6 \cos x_2 \in [-0.5574, 0.8],$$

$$z_3 = \frac{\sin x_2}{x_2} \in [0.8967, 1],$$

$$z_4 = x_6 \sin (2x_2) \in [-0.8, 0.8],$$

$$z_5 = x_5 \in [-0.6, 0.6],$$

from which weighing functions

$$\omega_0^i = \frac{\overline{z_i - z_i}}{\overline{z_i - \underline{z_i}}}$$
$$\omega_1^1 = 1 - \omega_0^i$$

are defined to produce MFs

$$h_i = h_{1+i_1+i_2 \times 2+\ldots+i_5 \times 2^4} = \prod_{j=1}^5 w_{i_j}^j(z_j)$$

The resulting model has the form

$$\dot{x}(t) = \sum_{i=1}^{32} h_i(z(t)) \left(A_i x(t) + B_i u(t) \right), \quad (30)$$

with $(A_i, B_i) = (f(x), g(x))|_{h_i=1}$.

Conditions in Theorem 3 were found feasible in the MATLAB LMI Toolbox (Gahinet *et al.*, 1995) for a time delay of $\tau = 0.27$ and decay rate $\sigma = 0.25$. The resulting PDC control law is (6) with 32 gains K_i , which, along with the MFs h_i , $i \in \{1, 2, ..., 32\}$, constitute the convex sum K_z . Here, the exponential estimates for initial condition $\phi = \begin{bmatrix} 0 & 0.57 & 0 & 0 & -0.4 & 0 & 0 \end{bmatrix}$ are

$$\begin{aligned} |x(t;\phi)|| &\leq \sqrt{\frac{\alpha_2}{\alpha_1}} e^{-\sigma t} ||\phi||_{\tau} \\ &= 46.6971 e^{-0.25t} ||\phi||_{0.27}, \end{aligned}$$

with a guaranteed cost of $J_0 = 16.4828$. The Lyapunov–Krasovskii functional matrices and some of the 32 gains are shown below.

The time evolution of the TRMS states under the time-delayed control law above is shown on the left in Fig. 1, and the control law is depicted on the right. It can be seen that, despite the time delay, stabilization as well as the exponential bound are achieved.

The TRMS employed for real time-implementation only provides states x_2 , x_3 , x_5 , and x_6 , which are measurements from the encoder sensors; the remaining states have to be estimated (Fee, 1998). As can be checked in the user's guide, states x_1 , x_4 , and x_7 can be filtered from the input torques; note that this task does not lead to algebraic loops if the input is delayed. Thus, real-time implementation of the simulation results above is shown in Fig. 2. The peaks presented in the figure are user-induced perturbations.

822

5. Conclusions

A novel approach to stability and stabilization of nonlinear systems with delayed multivariable inputs providing exponential estimates as well as a guaranteed cost of the system solutions has been presented. An exact convex representation of the system in a compact set of the state-space has been used altogether with a Lyapunov–Krasovskii functional to obtain sufficient conditions in the form of linear matrix inequalities, which are efficiently solved via convex optimization techniques. In contrast to other results on the subject, this development makes use of recent techniques such as Finsler's lemma in order to combine inequalities and restrictions in a single unified framework. The developed approach has been successfully implemented in real time on the twin rotor MIMO system.

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K_1 :	$= \begin{bmatrix} -3.3417 \\ 1.4272 \end{bmatrix}$	8.1422	-2.2709	-0.0257	-0.0234	0.0001	0.5179	
1	[1.4659	-2.8253	0.6360	-2.0600	-2.1259	-0.7830	31.8786] '	
	[_3 3136	8 0005	-2 2526	-0.0279	-0.0268	-0.0057	0 5569]	
K_9 :	$= \begin{vmatrix} 0.0100\\ 1.4599 \end{vmatrix}$	-2.7957	0.6340	-2.0073	-2.1000	-0.7624	31.0891,	
	L							
V	[-3.291]	3 8.0672	-2.2397	-0.0253	-0.0277	-0.0130	0.4945	
K_{17}	$= \begin{bmatrix} 1.4596 \end{bmatrix}$	-2.7905	0.6354	-2.0037	-2.0985	-0.7545	31.0708,	
K_{25}	$= \begin{bmatrix} -3.273 \end{bmatrix}$	0 8.0429	-2.2310	-0.0218	-0.0285	-0.0205	0.4122	
25	1.4660	-2.8019	0.6441	-2.0277	-2.1108	-0.7590	31.4627]'	
E F	8.1141 -	-12.5152	10.1272	-0.4417	-0.5756	-0.1370	12.3295	
-	12.5152	46.3667	-9.8052	0.5021	0.5912	0.2876	-6.5328	
1	0.1272 -	-9.8052	20.4008	0.1383	0.0581	-0.0395	-2.6478	
P = -	-0.4417	0.5021	0.1383	10.5371	5.0784	-3.3166	-119.3204	,
-	-0.5756	0.5912	0.0581	5.0784	10.3226	1.6848	-63.9367	
-	-0.1370	0.2876	-0.0395	-3.3166	1.6848	6.6901	35.6074	
L 1	2.3295 -	-6.5328	-2.6478 -	-119.3204	-63.9367	35.6074	1594.0950	
	E 0 0039	0.0003	0.0037	0.0057	0.0067	-0.0243	0.0001.7	
	0.0003	0.0003	-0.0001	0.0009	0.0021	-0.0050	0.0000	
	0.0037	-0.0011	0.0124	-0.0040	-0.0021	0.0113	-0.0001	
Q =	0.0057	0.0009	-0.0040	0.2355	0.0055	-0.2075	0.0185	
~	0.0067	0.0021	-0.0031	0.0055	0.0803	-0.0606	0.0023	
	-0.0243	-0.0050	0.0113	-0.2075	-0.0606	0.9222	0.0060	
	0.0001	0.0000	-0.0001	0.0185	0.0023	0.0060	0.0023	
	_						_	
R =	5.3827	0.2710	-2.4988	-0.5332	-0.0164	0.0340	-0.1191	
	0.2710	0.2200	-0.0152	-0.0533	-0.0029	-0.0180	-0.0025	
	-2.4988	-0.0152	1.4002	0.2484	0.0067	-0.0283	0.0597	
	-0.5332	-0.0533	0.2484	3.7296	-0.0178	0.1266	0.2588 .	
	-0.0164	-0.0029	0.0067	-0.0178	1.9919	-0.4440	0.0927	
	0.0340	-0.0180	-0.0283	0.1266	-0.4440	2.9497	0.0015	
	$\lfloor -0.1191$	-0.0025	0.0597	0.2588	0.0927	0.0015	0.0540	

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Fig. 1. State evolution of the TRMS under the control law (6) obtained via Theorem 3 with $\tau = 0.27$, $\sigma = 0.25$ (a). Time evolution of the control signals (b).



Fig. 2. State evolution of the TRMS under the control law (6) obtained via Theorem 3 with $\tau = 0.27$, $\sigma = 0.25$ (a). Time evolution of the control signals (b).

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amcs 826

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